### **HFT Alignment Procedures**

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- Introduction
- HFT Configuration System hierarchy
- (thoughts on) Proposed procedures
- Tools/Implementation (Jonathan)
- Plans, Timeline and Issues
- Summary

Alignment procedures review, BNL, Oct. 12, 2012

## Flowchart of Geometry/Survey/Alignment



\* VMC, STV ready

## Introduction

- Anything we build or touch or use needs Modeling, Survey and in-situ Alignment
  - i.e. versioning
- Survey will freeze position of sensors on sectors (PXL). Help also with sector on hemisphere (PXL?). For SSD/IST will freeze position of sensors on ladder and ladder shape
- For each yearly Run the in-situ position of major detector elements needs to be rechecked

## Reference System Hierarchy







## **General Layout**





### Reference systems - comments

- In general survey accuracy of critical components (relative pixel and/or sensor positions) expected to be better than acceptable values
- Will soon need surveyed positions of IDS targets
  - to build 'ideal' position Db
  - Sub-millimeter accuracies acceptable -> Tracks will fix them
- All this information is represented as matrices (position/orientation) of their center-of-gravity. These matrices are used to define Local to Global transforms

GEANT geometry can/should be synchronized with Realistic Volume hierarchy instead of the current 'patch-the-hit' scheme

- VMC environment will facilitate this

### Definitions

**Global Coordinates** 

### Local Coordinates



- Local v (along ladder) is fixed and along global z
- Local w (normal to wafer plane) is fixed (points away from the interaction point
- Local u (rphi on wafer plane) varies so it forms a RHS with v-ww

### Offline use of Geometry Info

- Local-to-Global transforms are done in terms of TGeoHMatrix
- This can be e.g. the center of a sensor or a pixel.
- n,d,t are unit vectors and  $\beta,\alpha,\gamma$  the corresponding rotation angles, RHS

TGeoHMatrix definition
$$\begin{pmatrix} x_G \\ y_G \\ z_G \\ 1 \end{pmatrix}$$
= $\begin{pmatrix} \hat{d}_x & \hat{n}_x & \hat{t}_x & d_x \\ \hat{d}_y & \hat{n}_y & \hat{t}_y & d_y \\ \hat{d}_z & \hat{n}_z & \hat{t}_z & d_z \\ 0 & 0 & 0 & 1 \end{bmatrix}$  $\begin{pmatrix} x_L \\ y_L \\ z_L \\ 1 \end{pmatrix}$ 

Transform example  

$$x_{G}^{i} = R \cdot x_{L}^{i} + T^{i}$$

$$x_{G} = \left(\hat{d}_{x} \cdot x_{L} + \hat{n}_{x} \cdot y_{L} + \hat{t}_{x} \cdot z_{L}\right) + d_{x}$$

### Local <-> Global transforms

#### OLD SSD

WG = Tpc2Global \* GL \* SG \* LS \* WLL; WaferInGlobal=Tpc2Magnet \*SsdinTpc\*SectorInSSD\*LadderInSector\*WaferInLadder

#### HFT SSD

WG = Tpc2Global \* GL \* LO \* WLL; WaferInGlobal=Tpc2Magnet \*IDS2Tpc\*Ladder2IDS\*WaferInLadder

#### HFT IST

WG = Tpc2Global \* GL \* PI \*LO \* WLL; WaferInGlobal=Tpc2Magnet \*IDS2Tpc\*PST2IDS\*Ladder2PST\*WaferInLadder

#### HFT PXL

PG = Tpc2Global \*GL \* PI \*DP \* SD \* WLL; PXLInGlobal=Tpc2Magnet\*IDS2Tpc\*PXL2IDS\*DShell2PXL\*Sector2DShell\*(Pxl-Sector)

# Alignment methods (outline only)

- There are 'Global' and 'Self' Alignment methods
  - Global uses mostly 'external' track information
  - Self uses mostly 'internal' track information
  - For HFT we propose a mix (more Self!)
- We have successful 'Global' methods already in place (SVT/SSD)
  TPC distortions, t0, 'track tof' etc is a problem
- In HFT system we have significant sensor overlap to make use of 'Self' alignment methods. We also have high precision PXL info with excellent sector rigidity, survey info, placement.
- We need to use this advantage

We lack a hardware monitoring system. Once detectors are installed we rely on survey and alignment software The hit-track residual  $\Delta x$  in the direction perpendicular to the axial strips is given by

$$\Delta x \equiv x_{track} - x_{hit} = \delta x + z \sin \beta + \tan \phi (\delta y + z \sin \alpha + x \sin \gamma) - f(\vec{B}, \phi)$$
(1)

and for the direction parallel to the axial strips (in double sided ladders)

$$\Delta z \equiv z_{track} - z_{hit} = \delta z + x \sin \beta + \tan \theta (\delta y + z \sin \alpha + x \sin \gamma)$$
(2)

The simplest approach to determining the alignment parameters is to use the means of the following histograms (for the  $\Delta x$  case):

- 1. the distribution of residuals integrated over y, z, and  $\phi$ , which gives  $\delta x$  directly,
- 2. the residual vs. z which gives  $\sin \beta$ ,
- 3. the residual vs.  $\tan \phi$  which gives  $\delta y$ ,
- 4. the residual/tan  $\phi$  vs. x which gives sin  $\gamma$ ,
- 5. and the residual/tan  $\phi$  vs. z which gives sin  $\alpha$ .

D.Chakraborty, J.D.Hobbs, D0 note Oct.13, 1999



The sequence to be followed for each detector is:
1) SSD Alignment: (TPC tracks Only) Global - SSD on Global and Sectors on Global; Local - SSD Ladders on Sectors;
2) SVT Alignment: (TPC+SSD hits on tracks) Global - SVT on Global and Shells on Global; Local - SVT Ladders on Shells; (Drift Velocities);
3) Consistency Check: (TPC+SSD+SVT hits on tracks) Global;Local (ladders);Drift Velocities;

- For alignment we use "good" (well defined) tracks fitted with the primary vertex. (e.g. NFP, pt cuts)
  - Use of primary tracks significantly improves precision of track predictions in HFT and reduces influence of systematics.
  - Good statistics is a must (up to a point)(see example in Jonathan's talk)(50-100K hits per wafer/sensor)
- In order to minimize TPC space-charge distortions, tracking errors (mismatches) and PXL pileup we will need to use low luminosity and low-medium multiplicity data as the alignment sample
- Method is iterative since it is precise for small deviations

### HFT Proposed Procedure:

Remember: PXL detector is a big asset (c.f. TPC)

### 1. Global Alignment of PXL

- Relative alignment of PXL sectors and halves using overlap region AND halves using Event vertex found by each half
- Relative alignment of PXL and TPC [TPC primary tracks]
  - Iterative->(PXL, PXL half, sector)
- Exact sequence/interplay needs to be determined
- 2. Primary tracks with TPC+PXL hits
  - Alignment of IST ladders with respect to PXL
- 3. Primary tracks with (All SSD) hits
  - Alignment of SSD ladders

### 4. Check

• We assume that sensors on ladder and ladders on sectors are pre-surveyed to specs 16

## Precision requirements for HFT alignment

- Pointing accuracy is ultimate figure of merit: DCA resolution (in bending XY =r $\phi$  plane:  $\sigma_{DCA}$ ), and resolution in non-bending plane:  $\sigma_z$ 
  - $\sigma^2_{\text{DCA}} = \sigma^2_{\text{vertex}} + \sigma^2_{\text{track}} + \sigma^2_{\text{MCS}}$  (the same for non-bending plane)
  - primary vertex resolution:  $\sigma_{vertex}$  ~ 3µm+(120 µm / JN<sub>ch</sub>); for central Au+Au collisions turns out to be ~5 µm
  - track pointing resolution:  $\sigma_{\text{track}} \sim 1.5 \sigma_{XY}$  [in our case, where  $\sigma_{XY}$  is intrinsic detector precision (~10µm)]  $\oplus$  alignment errors
  - multiple scattering (MCS):  $\sigma_{\text{MCS}}$  ~ 20 $\mu\text{m}$  /  $\beta\text{p}$  (GeV/c) (for thin PXL)

Overall mis-alignments of < 10  $\mu\text{m}$  or <MCS are acceptable

## DCA resolution



### •SVT/SSD example

- •With increasing no. of fitted Si points it is improved by ~ order of magnitude.
- •Contribution from tracking (constant term) is comparable with MCS @ 1 GeV/c

Number of Silicon Points fitted to track	σ <sub>χγ</sub> @1GeV/c (μm)
0 -  TPC only	3350
1 - 🛑 TPC+SSD	967
2 -  TPC+SSD+SVT	383
3 - • TPC+SSD +SVT	296
4 - TPC+SSD +SVT	281

## Tasks

- Need to finalize the PXL sensor representation in Db (prototype sector)
- Need to setup Data formats, code to deliver matrices etc
- Need to know/map the (realistic) error of every survey step
- Need to start simulations to determine alignment software performance
- Need to rework GEANT geometry synchronization (STV, VMC)
- Need to finalize SSD procedures and initialize/define IST ones
- Need to include gravitational sagging in SSD and IST (?) model
- Need to keep/use expertise around

## Plans/Timeline

Some of these efforts need to go in parallel

- It will take about a month or two to setup the chain and clean up the code for all HFT subsystems (current environment)
  - Includes software, Db structures, Hit, conventions
- We can do (some) tests in current environment or begin porting to VMC (with help)
- By the end of the year we would need to have defined and have established working interfaces to Survey for PXL
- Full chain ready to work with cosmics/data when available

Only then, when done, we can start looking at other packages

### Summary

- The building up of a working chain is coming along
- All 3 needed efforts are moving along (Geo, Sur, Al)
- Benefited enormously from previous experience as we hope to benefit from current experience
- A lot still needs to be done
- Target to have a working chain for data beginning of the year is not unrealistic



# References

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- 3. "Correcting for distortions due to ionization in the STAR TPC", G. Van Buren et al.,NIM A566:22-25,2006.
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- 5. "The STAR silicon strip-detector (SSD)", L.Arnold et al., NIM 2003 A499: 652, 2003.
- 6. "Alignment Strategy for the SMT Barrel Detectors", D.Chakborty, J.D.Hobbs, October 13, 1999. D0 Note (unpublished)
- 7. "Sensor Alignment by Tracks", V.Karimaki et al.,CMS CR-2004/009 (presented at CHEP 2003)
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- 9. http://phys.kent.edu/~margetis/STAR/HFT/Survey/SVT\_Alignment\_JPCSL.pdf

#### Small Scale Self-Alignment with the SVT

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$$\Delta A = -B\delta\phi_n - \delta x_d + v_{dn}[A\delta\phi_t - B\delta\phi_d + \delta x_n]$$
  
$$\Delta B = A\delta\phi_n - \delta x_t + v_{tn}[A\delta\phi_t - B\delta\phi_d + \delta x_n]$$

24 http://drupal.star.bnl.gov/STAR/comp/calib/svt/selfalign The hit-track residual  $\Delta x$  in the direction perpendicular to the axial strips is given by

$$\Delta x \equiv x_{track} - x_{hit} = \delta x + z \sin \beta + \tan \phi (\delta y + z \sin \alpha + x \sin \gamma) - f(\vec{B}, \phi)$$
(1)

and for the direction parallel to the axial strips (in double sided ladders)

$$\Delta z \equiv z_{track} - z_{hit} = \delta z + x \sin \beta + \tan \theta (\delta y + z \sin \alpha + x \sin \gamma)$$
(2)

$$\Delta A = -B\delta\phi_n - \delta x_d + v_{dn}[A\delta\phi_t - B\delta\phi_d + \delta x_n]$$
  
$$\Delta B = A\delta\phi_n - \delta x_t + v_{tn}[A\delta\phi_t - B\delta\phi_d + \delta x_n]$$

The simplest approach to determining the alignment parameters is to use the means of the following histograms (for the  $\Delta x$  case):

1. the distribution of residuals integrated over y, z, and  $\phi$ , which gives  $\delta x$  directly,

- the residual vs. z which gives sin β,
- 3. the residual vs.  $\tan \phi$  which gives  $\delta y$ ,
- 4. the residual/tan  $\phi$  vs. x which gives sin  $\gamma$ ,
- 5. and the residual/tan  $\phi$  vs. z which gives sin  $\alpha$ .

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A. Appendix. Jacobian of measured hit position deviation from predicted track ones with respect to misalignment parameters.

- 1. Misalignment of the detector in Global Coordinate System (GCS)
- $\vec{j} = (j_x, j_y, j_z)$  track direction cosinuses in GCS on measurement plane,
- $\vec{x} = (x, y, z)$  track prediction in GCS on measurement plane,
- \$\vec{x}\_{hit}\$ = (\$x\_{hit}\$, \$y\_{hit}\$, \$z\_{hit}\$) hit position in GCS on measurement plane,
- $\vec{v} = (v_x, v_y, v_z)$  direction of perpendicular to measurement plane in GCS,
- Δ
   <sup>−</sup> = (Δ<sub>x</sub>, Δ<sub>y</sub>, Δ<sub>z</sub>, Δ<sub>α</sub>, Δ<sub>β</sub>, Δ<sub>γ</sub>) misalignment parameters: shift and rotation with respect to X,Y,Z axises, respectively.
- 2. Misalignment of the detector in Local Coordinate System (LCS)
- $\vec{u} = (u, v, w \equiv 0)$  track prediction in LCS on measurement plane.
- +  $(t_u, t_v)$  track direction tangenses in Local Coordinate system (LCS) on measurement plane.
- $\vec{u}_{hit} = (u_{hit}, v_{hit})$  hit position in LCS on measurement plane,
- $\vec{\delta} = (\delta_u, \delta_v, \delta_w, \delta_\alpha, \delta_\beta, \delta_\gamma)$  misalignment parameters, shift and rotation with respect to local u,v,w axises, respectively.

$$ec{u}_{hit} - ec{u} = \mathbf{L} \cdot ec{\delta} = egin{pmatrix} -1 & 0 & t_u & t_u v & -t_u u & v \ 0 & -1 & t_v & t_v v & -t_v u & -u \end{pmatrix} ec{\delta}$$

•  $(u_{hit} - u) = -\delta_u + t_u(\delta_w + v\delta_\alpha - u\delta_\beta) + v\delta_\gamma;$  $(v_{hit} - v) = -\delta_v + t_v(\delta_w + v\delta_\alpha - u\delta_\beta) - u\delta_\gamma;$ 26